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# GUIDELINES FOR THE APPROVAL OF FIXED WATER-BASED FIRE-FIGHTING SYSTEMS FOR RO-RO SPACES AND SPECIAL CATEGORY SPACES EQUIVALENT TO THAT REFERRED TO IN RESOLUTION A.123(V)

- The Committee, at its eighty-fourth session (7 to 16 May 2008), having considered the proposal by the Sub-Committee on Fire Protection at its fifty-second session, approved the Guidelines for the approval of fixed water-based fire-fighting systems for ro-ro spaces and special category spaces equivalent to that referred to in resolution A.123(V), as set out in the annex.
- Member Governments are invited to apply the annexed Guidelines when approving fixed water-based fire-fighting systems for ro-ro spaces and special category spaces on or after 9 May 2008 and bring them to the attention of ship designers, shipowners, equipment manufacturers, test laboratories and other parties concerned.
- This circular supersedes MSC/Circ.914.

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#### **ANNEX**

# GUIDELINES FOR THE APPROVAL OF FIXED WATER-BASED FIRE-FIGHTING SYSTEMS FOR RO-RO SPACES AND SPECIAL CATEGORY SPACES EQUIVALENT TO THAT REFERRED TO IN RESOLUTION A.123(V)

#### 1 GENERAL

These Guidelines have been developed in recognition of reasonable and realistic performance-based requirements for fixed water-based fire-fighting systems for ro-ro spaces and special category spaces.

These Guidelines and the fire tests are intended for closed ro-ro spaces and special category spaces defined by SOLAS regulations II-2/3.12 and II-2/3.46, respectively. Deluge systems can be applied on open ro-ro spaces when the actual wind condition is taken into consideration. Systems using automatic sprinklers are only permitted for closed ro-ro and special category spaces or other spaces where wind conditions are not likely to affect system performance.

#### 2 **DEFINITIONS**

- 2.1 Area of operation is a design area for wet-pipe, automatic sprinkler system (to be determined for each system by the test procedure described in the appendix to these Guidelines).
- 2.2 Deluge system, automatic and manual release is a system employing open nozzles attached to a piping system connected to a water supply through a valve that can be opened by signals from a fire detection system and by manual operation. When this valve is opened, water flows into the piping system and discharges from all nozzles attached thereto.
- 2.3 Deluge system, manual release is a system employing open nozzles attached to a piping system connected to a water supply through a valve that is opened by manual operation. When this valve is opened, water flows into the piping system and discharges from all nozzles attached thereto.
- 2.4 *Dry pipe system* is a system employing automatic sprinklers attached to a piping system containing air or nitrogen under pressure, the release of which (as from the opening of a sprinkler) permits the water pressure to open a valve known as a dry pipe valve. The water then flows into the piping system and out of the opened sprinklers.
- 2.5 *Fire control* limits the size of a fire by distribution of water so as to decrease the heat release rate, while controlling gas temperatures and pre-wetting adjacent combustibles and/or reducing heat radiation to avoid structural damage.
- 2.6 *Fire suppression* is the sharp reduction of the heat release rate of a fire and the prevention of regrowth.
- 2.7 Preaction system is a system employing automatic sprinklers attached to a piping system containing air that may or may not be under pressure, with a supplemental detection system installed in the same area as the nozzles or sprinklers. Actuation of the detection system opens a valve that permits water to flow into the piping system and to be discharged from any sprinklers that have operated.

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- 2.8 *Water-based extinguishing medium* is fresh water or seawater with or without additives mixed to enhance fire-extinguishing capability.
- 2.9 Wet pipe, automatic sprinkler system is a system employing automatic sprinklers attached to a piping system containing water and connected to a water supply so that water discharges immediately from sprinklers opened by heat from a fire.

#### 3 PRINCIPAL REQUIREMENTS

- 3.1 The system may be automatically activated, manually activated or automatically activated with manual release capabilities. Automatic activation should be approved by the Administration, taking into account the implications of such activations.
- 3.2 The system should be capable of fire suppression and control and be tested to the satisfaction of the Administration in accordance with the appendix to these Guidelines.
- 3.3 The capacity of the system water supply should be sufficient for the total simultaneous coverage of the hydraulically most demanding area defined by the minimum coverage area of table 3-1 and the vertically applicable area as defined in paragraph 3.5, and the requirements of paragraph 3.4 below.

Table 3-1

Type of system (Definition number)	Minimum coverage area
A. Wet pipe, automatic sprinkler heads (2.9)	280 m <sup>2</sup> or area of operation as defined in the fire tests – whichever is larger
B. Deluge system, automatic <sup>1</sup> and manual release (2.2)	280 m <sup>2</sup> (as per paragraph 3.6) and the overlapping or adjacent section as defined by paragraph 3.4 <sup>2</sup>
C. Deluge system, manual release (2.3)	2 sections each of min 20 m x w <sup>2,3</sup>
D. Other systems (2.4, 2.7)	Equivalent to the above systems and to the satisfaction of the Administration

# Notes:

- The automatic release should comply with the requirements of paragraphs 4.1 to 4.5.
- The pump should be sized to cover the largest sections for type B systems and the two largest horizontally adjacent sections for type C systems.
- Width of cargo space (measured as distance between tight steel divisions).
- 3.4 The section arrangement for a deluge system with automatic and manual release (system B) should be such that a fire in any location of the border zone between two or more sections would be completely surrounded by activated spray heads, either by activating more than one section or by overlapping sections (whereby two or more sections cover the same area in the vicinity of the border between sections). In case of overlapping sections, such overlap should be a minimum of two times the required spray head spacing of the section in question or five metres, whichever is larger. These overlapping sections need not comply with the minimum width and length requirements of paragraph 3.6 below.

- 3.5 Vertically the applicable area of all decks, including hoistable decks or other intermediate decks, between reasonably gas-tight steel decks (or equivalent materials), should be included for simultaneous coverage (example: with one hoistable deck, both the layer above and below this deck with a dimensioning area complying with table 3-1 should be included in the water supply calculations). Decks with ramps are accepted as reasonably gas-tight decks, assuming that the ramps are always in their closed position at sea and the ramps and the decks which these ramps are part of are reasonably gas-tight.
- 3.6 The system should be divided into sections, each with its own section valve. The length of a section (along the lanes) should not be less than 20 m and the width of the section should not be less than 14 m. Further, the sections need not be longer or wider than the distance between reasonably gas-tight steel bulkheads (or equivalent materials). The maximum size of a section on any single deck should be 48 m multiplied with width of cargo space (measured as distance between tight steel divisions). Vertically one section can cover up to three decks.
- 3.7 Each section should be capable of being isolated by one section control valve. The section control valves should be located outside the protected space, be readily accessible, independent of the protected spaces and their locations should be clearly and permanently indicated. It should be possible to manually open and close the section control valves either directly on the valve or via a control system routed outside the structural fire protection of the protected spaces. Means should be provided to prevent the operation of the section control valves by an unauthorized person.
- 3.8 The piping system should be sized in accordance with a hydraulic calculation technique such as the Hazen-Williams hydraulic calculation technique\* and the Darcy-Weisbach hydraulic calculation technique, to ensure availability of flows and pressures required for correct performance of the system. The design of the system should ensure that full system pressure is available at the most remote nozzle in each section within 60 s of activation.
- 3.9 The system supply equipment should be located outside the protected spaces and all power supply components (including cables) should be installed outside of the protected space. The electrical components of the pressure source for the system should have a minimum rating of IP 54.
- 3.10 The system should be provided with a redundant means of pumping or otherwise supplying a water-based extinguishing medium to the system. The capacity of the redundant means should be sufficient to compensate for the loss of any single supply pump or alternative source. Failure of any one component in the power and control system should not result in a reduction of the automatic release capability or reduction of required pump capacity by more than 50% in case of automatic sprinklers and 100% in case of open head systems. However, systems requiring an external power source need only be supplied by the main power source. Hydraulic calculations should be conducted to assure that sufficient flow and pressure are delivered to the hydraulically most demanding section both in normal operation and in the event of the failure of any one component.

Where the Hazen-Williams Method is used, the following values of the friction factor *C* for different pipe types which may be considered should apply:

Pipe type	<u>C</u>
Black or galvanized mild steel	100
Copper and copper alloys	150
Stainless steel	150

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- 3.11 The system should be fitted with a permanent sea inlet and be capable of continuous operation during a fire using seawater.
- 3.12 The system and its components should be designed to withstand ambient temperatures, vibration, humidity, shock, impact, clogging and corrosion normally encountered.
- 3.13 The system and its components should be designed and installed based on international standards acceptable to the Organization\*. The nozzles should be manufactured and tested based on the relevant sections of appendix A to MSC/Circ.1165.
- 3.14 The nozzle location, type of nozzle and nozzle characteristics should be within the limits tested to provide fire suppression and control as referred to in paragraph 3.2. In addition, nozzles should be located to protect spaces above and below intermediate decks, hoistable decks and ramps. Nozzles below hoistable decks should be capable of protecting all applicable heights.
- 3.15 System designs should be limited to the use of the maximum and minimum temperature ratings of the thermally sensitive fire detection devices tested to provide fire suppression and control as referred to in paragraph 3.2.
- 3.16 Activation of the system should give a visual and audible alarm at a continuously manned station. The visual and audible alarms should be activated when for instance an automatic sprinkler operates or when a section valve is opened. The alarm in the continuously manned station should indicate the specific section of the system that is activated. The system alarm requirements described within this paragraph are in addition to, and not a substitute for, the detection and fire alarm system required by SOLAS regulation II-2/20.4.
- 3.17 A means for testing the automatic operation of the system and, in addition, assuring the required pressure and flow should be provided.
- 3.18 If the system is pre-primed with water containing a fire suppression enhancing additive and/or an antifreeze agent, periodic inspection and testing, as specified by the manufacturer, should be undertaken to assure that their effectiveness is being maintained. Fire suppression enhancing additives should be approved for fire protection service by an independent authority. The approval should consider possible adverse health effects to exposed personnel, including inhalation toxicity.
- 3.19 Wet pipe systems on board vessels that can operate in areas where temperatures below 0°C can be expected, shall be protected from freezing either by having temperature control of the ro-ro space, heating coils on pipes, antifreeze agents or other equivalent measures.
- 3.20 Operating instructions for the system should be displayed at each operating position.

<sup>\*</sup> Pending the development of International Standards acceptable to the Organization, national standards as prescribed by the Administration should be applied.

- 3.21 Installation plans and operating manuals should be supplied to the ship and be readily available on board. A list or plan should be displayed showing spaces covered and the location of the zone in respect of each section. Instructions for testing and maintenance should be available on board.
- 3.22 Spare parts and operating and maintenance instructions should be provided as recommended by the manufacturer. In the case of automatic sprinkler systems, the total number of spare sprinkler heads for each type of sprinklers should be 6 for the first 300, 12 for the first 1,000.
- 3.23 Where automatically operated fire-fighting systems are installed, a warning notice should be displayed outside each entry point stating the type of medium used and the possibility of automatic release
- 3.24 All installation, operation and maintenance instruction/plans for the system should be in the working language of the ship. If the working language of the ship is not English, French, nor Spanish, a translation into one of these languages should be included.

# 4 DETAIL REQUIREMENTS – FIRE DETECTION AND FIRE CONFIRMATION (SYSTEM B)

- 4.1 For systems of type B (see table 3-1) an efficient fire detection and fire confirmation system covering all parts of the ro-ro or special category spaces should be provided.
- 4.2 The fire detection system should consist of flame detectors and smoke detectors of approved types. The flame detectors should be installed under fixed continuous decks according to the limitation and application defined by the maker and the approval certificate. The smoke detector arrangement shall comply with the International Code for Fire Safety Systems (FSS Code). Smoke detectors with a spacing not exceeding 11 m should be installed under hoistable ramps.
- 4.3 A colour TV monitoring system should cover all parts of the ro-ro or special category spaces. Cameras need not be installed below hoistable decks if the camera arrangement can identify smoke (confirm fire) based on positions under a fixed continuous deck.
- 4.4 The relevant section of the deluge system should be automatically released when two detectors covering this area activate. Systems being released when only one detector activates may also be accepted. The automatic release should not prevent manual operation (both opening and closing) of the section valves. The automatic release may be disconnected during on- and off-loading operations, provided that this function is automatically re-connected after a pre-set time being appropriate for the operations in questions.
- 4.5 All release controls for the deluge system, monitor(s) for the CCTV system and the control panel (or an indication panel) for the fire detection system should be available and grouped together in a continuously manned control station.

#### **APPENDIX**

# TEST METHOD FOR FIXED WATER-BASED FIRE-FIGHTING SYSTEMS FOR RO-RO SPACES AND SPECIAL CATEGORY SPACES

#### 1 SCOPE

- 1.1 This test method is intended for evaluating the effectiveness of fixed water-based fire-fighting systems installed in ro-ro spaces and special category spaces with deck heights up to and including 5 m and/or up to and including 2.5 m.
- 1.2 The test programme has two objectives:
  - .1 establishing nozzle location, nozzle characteristics, minimum water delivery rate and minimum water pressure for systems which will provide the required level of system response time, suppression and control; and
  - .2 establishing the minimum area of operation of the system for the purpose of determining hydraulic design requirements for wet pipe, dry pipe and preaction systems.

#### 2 GENERAL REQUIREMENTS

# 2.1 Sampling

The nozzles and other components to be tested should be supplied by the manufacturer together with design and installation criteria, operational instructions, drawings and technical data sufficient for the identification of the components.

#### 2.2 Tolerances

Unless otherwise stated, the following tolerances should apply:

.1 length:  $\pm 2\%$  of value;

.2 volume:  $\pm$  5% of value;

.3 pressure:  $\pm 3\%$  of value; and

.4 temperature:  $\pm 2\%$  of value.

# 2.3 Observations

The following observations should be made during and after each test:

- .1 time of ignition;
- .2 activation time of first nozzle;
- .3 time when water flows out through first nozzle;

- .4 time when water flow is shut off;
- .5 time when the test is terminated; and
- .6 total number of activated nozzles.

#### 2.4 Test hall and environmental conditions

The test hall where the tests are conducted should have a minimum floor area of 300 m<sup>2</sup> and a ceiling height in excess of 8 m. The test hall may be equipped with a forced ventilation system, or be natural ventilated, in order to ensure that there is no restriction in air supply to the test fires. The test hall should have an ambient temperature of between 10 and 25°C at the start of each test.

#### 2.5 Measurement equipment

Temperatures should be measured using plain K-type thermocouple wires not exceeding 0.5 mm in diameter. The thermocouple head should be protected against direct water impingement, e.g., by tin cans.

System water pressure should be measured by using suitable equipment. Total water flow rate should be determined by a direct measurement or indirectly by using the pressure data and k factor of the nozzles.

The measurements should be made continuously throughout the tests.

#### 2.6 System operational conditions

The tests should simulate the conditions of an actual installed system regarding objectives such as time delays between the activation of the system and minimum system water pressure or water delivery. In addition, the use of a pre-primed fire suppression enhancing additive, if applicable, should be taken into account

#### 3 DETERMINATION OF FIRE SUPPRESSION AND CONTROL CAPABILITIES

#### 3.1 Principle

These test procedures test the effectiveness of a water-based fire-fighting system against two different scenarios: a cargo fire in a simulated freight truck, and a passenger vehicle fire.

#### 3.2 Fire source

- 3.2.1 The primary fire source for both scenarios consists of EUR standard wood pallets (ISO 6780:2003), stored inside with the moisture content of  $14 \pm 2\%$ . Figure 3.2.1 shows details of a EUR pallet.
- 3.2.2 Plywood panels made of pine or spruce are used as targets. The panels should be approximately 12 mm thick. The ignition time of the panel should not be more than 35 s and the flame spread time at 350 mm position should not be more than 100 s as measured in accordance with resolution A.653(16).

# 3.2.3 For ignition, commercial heptane is to be applied.

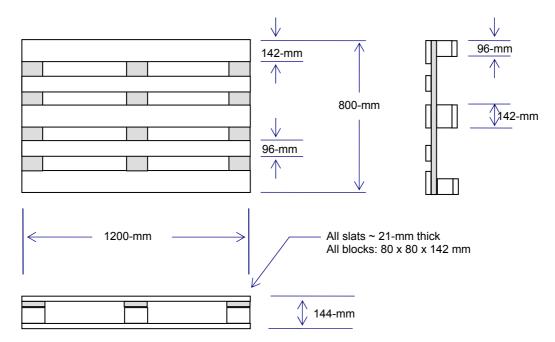


Figure 3.2.1 – Typical dimensions of the standard EUR pallet

# 3.3 Apparatus

#### 3.3.1 Test area

The tests should be conducted in a test hall as specified in paragraph 2.4 above, under a flat, smooth, non-combustible ceiling of at least 100 m<sup>2</sup>. There should be at least a 1 m space between the perimeters of the ceiling and any wall of the test hall.

# 3.3.2 *Fire scenario 1: cargo fire in a simulated freight truck* (see figures 3.3.2.1 to 3.3.2.3)

- 3.3.2.1 The primary fuel package consists of 112 wood pallets arranged in an array of 2 (wide) x 7 (high) x 8 (long) and raised up on a level of 2.8 m so that the top level of the fuel package is at 3.8 to 3.9 m above the floor.
- 3.3.2.2 The support frame for the wood pallet array of paragraph 3.3.2.1 should be constructed using open steel racks. The wood pallet piles should be standing freely on horizontal steel beams without any solid bottoms.
- 3.3.2.3 The fuel pallet array should be half-shielded by a 4.5 m long, 2.6 m wide steel plate (thickness at least 2 mm) at 4 m height. The plate should be properly fixed so that during a test it does not bend to provide an unobstructed passage of water onto the fuel package.
- 3.3.2.4 Plywood panel targets (acting also as obstructions) of dimensions 3.6 m (wide) x 2.4 m (high) should be arranged symmetrically on both sides of the fuel package at 1 m distance so that the top edge is at the same level as the top level of the wood pallet array.

3.3.2.5 The fire should be ignited by two steel trays centrally located under the fuel package as shown in figures 3.3.2.1 to 3.3.2.3. The square trays are 25 cm high and 0.1  $m^2$  of free surface area. The trays should be filled with water and 1 l of heptane so that the free rim height above the liquid surface is 4 cm. The distance between the bottom of the wood pallet piles and liquid surface is 29 cm.

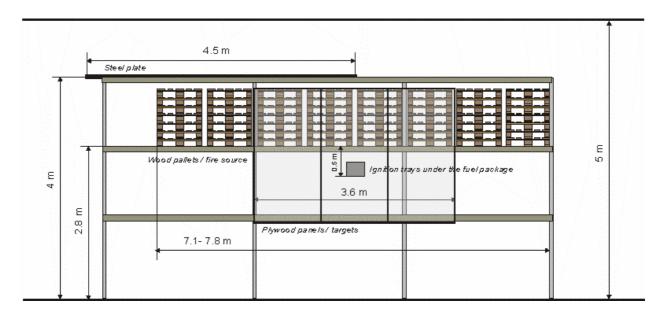


Figure 3.3.2.1 – Side view of the cargo fuel package in a simulated truck

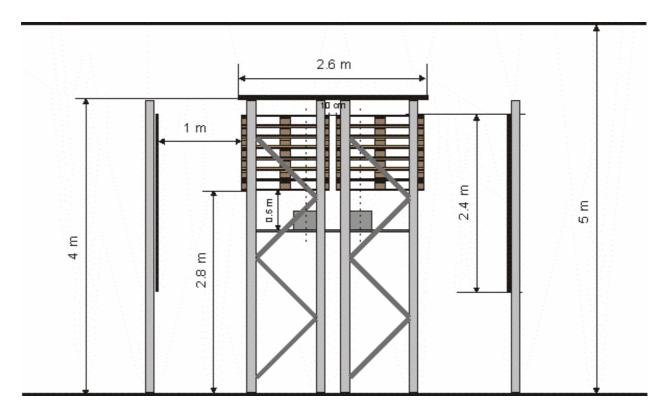


Figure 3.3.2.2 – End view of the cargo fuel package in a simulated truck

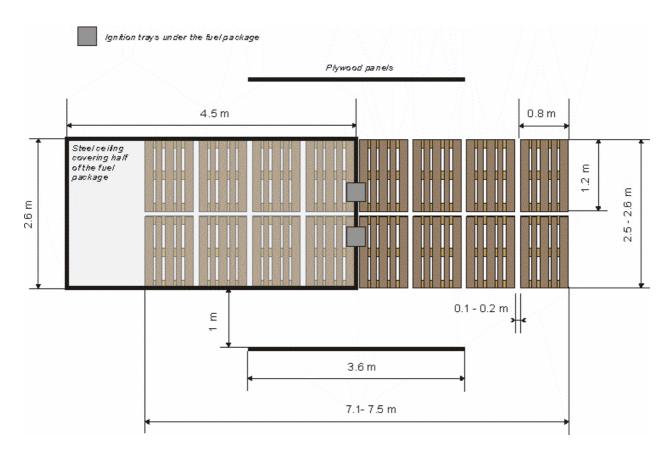


Figure 3.3.2.3 – Top view of the cargo fuel package in a simulated truck

- 3.3.3 *Fire scenario 2: passenger vehicle fire* (see figures 3.3.3.1 and 3.3.3.2)
- 3.3.3.1 The primary fuel package consists of 12 wood pallets arranged in an array of 1 pallet (wide) x 6 pallets (high) x 2 pallets (long) constructed inside a passenger vehicle mock-up.
- 3.3.3.2 The passenger vehicle mock-up is constructed of nominally 2 mm steel.
- 3.3.3.3 Plywood panel targets (acting also as obstructions) of dimensions 1.2 m (wide) x 1.75 m (high) should be arranged symmetrically on both sides of the mock-up at 0.6 m distance so that the top edge is at the same level as the top level of the mock-up car.
- 3.3.3.4 The fire should be ignited by a steel tray centrally located under the fuel package as shown in figures 3.3.3.1 and 3.3.3.2. The square tray is 10 cm high and 0.1  $m^2$  of free surface area. The tray should be filled with water and 1 l of heptane so that the free rim height above the liquid surface is 4 cm.

# 3.4 Nozzle positioning

Nozzles should be installed in an array at the ceiling level in accordance with the manufacturer's design and installation criteria. Tests should be repeated with three different relative locations between the nozzle array and the fuel package, i.e., centre of ignition under one nozzle, between two nozzles and between four nozzles, as shown in figure 3.4.1.

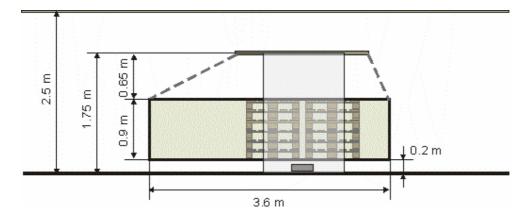


Figure 3.3.3.1 – Side view of the passenger vehicle fuel package (The dashed lines visualize the shape of a car; the ceiling plate is to be fixed in its location as found most practical)

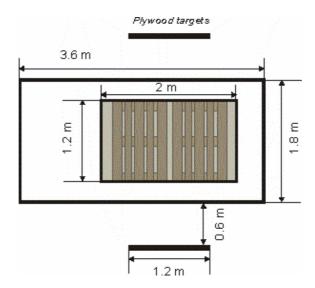


Figure 3.3.3.2 – Top view of the passenger vehicle fuel package

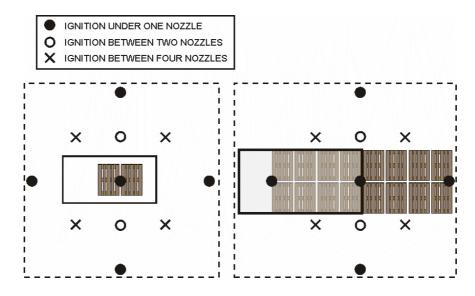


Figure 3.4.1 – Nozzle positioning in the two scenarios

# 3.5 Instrumentation

Instrumentation for the continuous measuring and recording of test conditions should be employed. At least the following measurements should be made:

- .1 gas temperature at 7.5 cm below the ceiling at locations shown in figure 3.5.1;
- .2 gas temperature at the targets to indicate ignition of targets as shown in figure 3.5.2; and
- .3 system water pressure near the centre of the piping array.

System water flow rate should be defined with suitable means for the system.

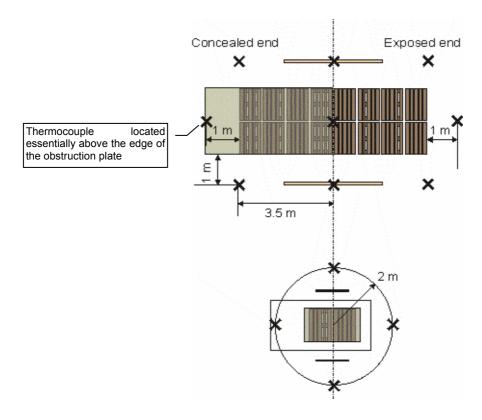


Figure 3.5.1 – Thermocouple locations in the two scenarios\*

<sup>\*</sup> For the truck fuel package the three locations at both ends are used for acceptance evaluation, the three locations at and around the centre of ignition are for safety purposes to define during the test whether the ceiling is at danger. For the passenger car fuel package all four locations are used for acceptance evaluation.

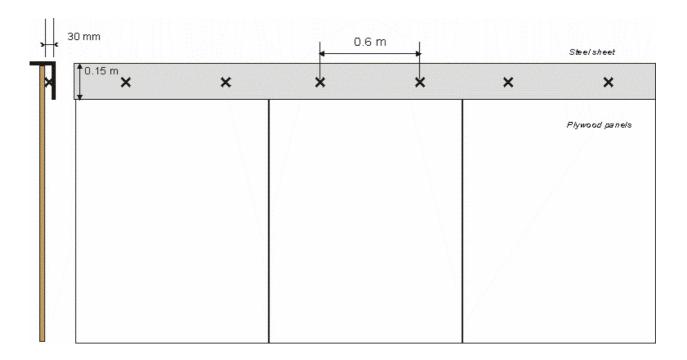


Figure 3.5.2 – Thermocouple locations at the plywood targets for determining ignition of targets\*

# 3.6 Test programme and test procedure

# 3.6.1 *Test programme*

Tests should be conducted at the minimum system water pressure at the minimum distance between the lowest part of the nozzles and the ceiling, as specified by the manufacturer.

Three tests should be conducted at ceiling heights 5 m and/or 2.5 m, with different nozzle grid locations relative to the fuel package as specified in figure 3.4.1.

#### 3.6.2 *Test procedure*

Prior to starting the test the moisture content of the fuel package should be measured at several locations along the full package with a probe-type moisture meter and the results should be reported.

The actual test procedure for all tests is as follows:

.1 the water pressure used at the start of the test should be set at the minimum value for the system specified by the manufacturer, flowing six open nozzles. If more than six nozzles operate during the test, the water supply pressure should be adjusted accordingly, to keep the required minimum system water pressure;

<sup>\*</sup> A thin (about 1 mm) steel sheet is bent on top of the plywood panels as shown in the figure. Plain charring of panels is seen as a sharp edge between the black charring on the exposed surface and intact surface under the metal sheet. When ignited in flames charring is seen also under the sheet and verified by significant increase in the gas temperature under the metal sheet.

- .2 the tray should be filled with 1 *l* litre of heptane on the water base as described in paragraph 3.3.2.5 or 3.3.3.4;
- .3 the measurements are started;
- .4 the flammable liquid pool fire/s should be lit by means of a torch or a match;
- .5 the fire should be allowed to burn freely for a period of 2.5 min;\*
- .6 the test is continued for 30 min after system activation;
- .7 any remaining fire should be manually extinguished; and
- 8 the test is terminated.

# 3.7 Acceptance criteria

The principal acceptance criteria are based on the following factors:

- .1 gas temperatures measured at locations not directly affected by impinging flames;
- .2 damage to the fuel package; and/or
- .3 ignition of targets.
- **Note 1**: Damage to the fuel package is defined by the fraction of charring of the full package. The damage to each individual wood pallet should be evaluated separately and the total fraction calculated based on the detailed results. Totally black, i.e., totally charred pallet is denoted as 100% damage of the pallet (even though the pallet may have maintained its shape) and totally intact pallet is denoted as 0% damage. Partially charred pallets should be visually evaluated. Proper and adequate photographs of the damaged fuel package should be included in the test report.
- **Note 2**: Ignition of targets is defined by the method described in figure 3.5.2, if the visibility during the test is such that it cannot be visually observed.

#### 3.7.1 Fire scenario 1: cargo fire in a simulated freight truck (ceiling height 5 m)

The following four criteria should be met:

.1 after system activation the maximum five minute average at any of the three measurement locations at the exposed end of the fuel package should not exceed 300°C;

If automatic sprinklers activate already during the 2.5 min pre-burn period, feeding water to the system should be delayed till after the 2.5 min.

- .2 after system activation the maximum five minute average at any of the three measurement locations at the concealed end of the fuel package should not exceed 350°C;
- .3 total damage to the wood pallet array should not exceed 45% as defined after the test; and
- .4 the plywood targets should not ignite during the test.

# 3.7.2 Fire scenario 2: passenger vehicle fire

The following two criteria should be met:

- .1 after system activation the maximum five minute average at any of the four measurement locations should not exceed 350°C; and
- .2 the plywood targets should not ignite during the test.

#### 4 DETERMINATION OF AREA OF OPERATION

Both fire scenarios include hidden fires that burn intensely throughout the tests. The suppression tests as defined in paragraph 3.6.1 can be applied in establishing the area of operation of wet pipe, dry pipe and pre-action systems. The evaluation is based on the test with the largest number of nozzles activating.

The ceiling area of 100 m<sup>2</sup> as defined in paragraph 3.3.1 most likely is not sufficient for defining the area of operation. The ceiling should be large enough to allow installation of a sufficient number of nozzles so that it is unambiguous that the nozzles activating truly represent the maximum number of active nozzles

The area of operation is determined by multiplying the largest number of nozzles activating in the tests by two and defining the corresponding coverage area.

#### 5 TEST REPORT

The test report should, as a minimum, include the following information:

- .1 name and address of the test laboratory;
- .2 date of issue and identification number of the test report;
- .3 name and address of applicant;
- .4 name and address of manufacturer or supplier of the nozzles;
- .5 test method and purpose;
- .6 nozzle identification;
- .7 description of the tested nozzles and system performance;

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- .8 detailed description of the test set-up including drawings and photos of the fuel package and targets before and after the tests;
- .9 date of tests;
- .10 measured nozzle pressure and flow characteristics;
- .11 identification of the test equipment and used instruments;
- .12 test results including observations and measurements made during and after the test;
- .13 deviations from the test method;
- .14 conclusions; and
- .15 date of the report and signature.